

N/1  
SSR-107  
(TN-AP-67-279)

GPO PRICE \$ \_\_\_\_\_

CSFTI PRICE(S) \$ \_\_\_\_\_

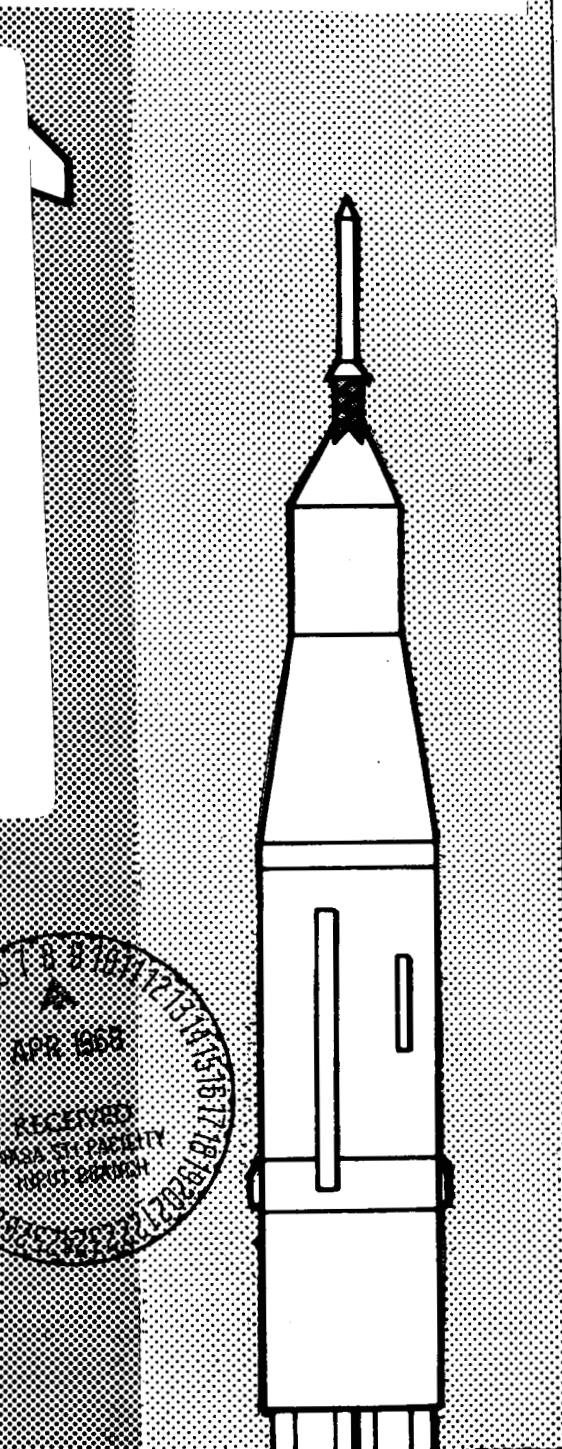
Hard copy (HC) 3.00

Microfiche (MF) \_\_\_\_\_

ff 653 July 65

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3  
(CODE)  
3  
(CATEGORY)

68 - 4113  
027  
(PAGES)  
093656  
(NASA CR OR TMX OR AD NUMBER)  
FACILITY FORM NO. 100-67



## AAP-1A LAUNCH VEHICLE PERFORMANCE AND PRELIMINARY RANGE SAFETY ANALYSES

Volume 2 RANGE SAFETY

CONTRACT NAS8-4016  
SCHEDULE II, VEHICLE  
SYSTEMS INTEGRATION

SPACE DIVISION



CHRYSLER  
CORPORATION

SSR-107  
(TN-AP-67-279)

AAP-1A LAUNCH VEHICLE PERFORMANCE AND PRELIMINARY RANGE SAFETY ANALYSES  
VOLUME 2 - RANGE SAFETY

NOVEMBER 1967

BY

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## PREFACE

This technical note consists of two volumes. Volume 1 documents eight nominal trajectories associated with the two stage uprated Saturn IB-AAP-1A mission (SA-207 CSM configuration). This volume, Volume 2, contains data and results of a preliminary range safety analysis applicable to the trajectories documented in Volume 1. The analysis documented herein has been scoped to meet the requirements of the range control office and was accomplished under MSFC-1, Amendment 38, SSR-107 issued 13 September 1967, and entitled "AAP-1A Launch Vehicle Performance and Preliminary Range Safety Study". The scheduled delivery date for the document and two cape magnetic tapes is 13 November 1967.

## SUMMARY

This volume presents range safety data and results for an uprated Saturn IB (AS-207/CSM) configuration into an 87 x 140 n. mi. elliptical orbit and is related to the AAP-1A mission. Generalized range safety data are contained in TR-AP-66-1. Certain data have been compiled on magnetic tapes in the format specified by the range control office.

Eight nominal trajectories were developed for this study - a northeast launch and a southeast launch for each of four orbit inclinations. Associated with orbit inclinations of 50°, 45°, 40°, and 35° are northeast flight azimuths of 45°, 51.3°, 57.2°, and 66.7°, respectively and southeast flight azimuths of 131.9°, 125.3°, 118.25°, and 110.1°, respectively.

The in-plane length of S-IB stage impact containment zones related to both northeast and southeast trajectories varies between 44.3 km and 47.5 km. The in-plane length of ullage-rocket cases impact containment zones varies between 58.1 km and 63.2 km.

Since land masses are overflowed, an impact and casualty probability study was conducted. Dwell times for the continental land masses overflowed vary from 6.76 to 8.68 seconds for the northeast launches and from 0.37 to 93.28 seconds for the southeast launches. For the northeast launches, probability of impact varies from  $4.22 \times 10^{-4}$  to  $5.42 \times 10^{-4}$  and casualty probability varies from  $3.47 \times 10^{-6}$  to  $5.12 \times 10^{-5}$ . For the southeast launches, probability of impact varies from  $2.29 \times 10^{-5}$  to  $5.82 \times 10^{-3}$  and casualty probability varies from  $1.19 \times 10^{-6}$  to  $2.78 \times 10^{-5}$ .

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## Section 1.0 - INTRODUCTION

The purpose of SSR-107, with respect to range safety analysis, is to determine Saturn IB in-plane flight corridors for northeast and southeast launches related to orbital inclinations of 50°, 45°, 40° and 35°, respectively, in order that the Range may assess the potential hazards involved in such flights. Volumes 1 and 2 of this technical note, along with the data compiled on two associated cape magnetic tapes, document the work done to satisfy SSR-107.

A description of the study requirements delineated in the SSR follows.

- A. Use a two stage uprated Saturn IB launch vehicle (SA-207) with a CSM configuration for insertion into 87 x 140 n. mi. elliptical orbits having inclinations of 50°, 45°, 40° and 35° for both northeast and southeast launches, respectively.
- B. Generate a nominal, a  $3\sigma$  maximum, and a  $3\sigma$  minimum trajectory for each launch azimuth.
- C. Prepare the data in report form and on two cape magnetic tapes in the proper format as specified by the range office.

Contained herein are the expected  $\pm 3\sigma$  in-plane (referred to as maximum and minimum, respectively) trajectory deviations from the intended flight path; data related to the expected impacts of the expended S-IB stage and ullage-rocket cases; and downrange land impact and casualty probabilities for each flight azimuth. The cape magnetic tapes associated with this analysis are CCSD Reel No. 4194 containing data for the northeast launches and CCSD Reel No. 0895 containing data for the southeast launches.

## Section 2.0 - NORTHEAST LAUNCH AZIMUTHS

Formal range safety data requirements are defined for the launch agency by the Deputy Commander of tests (Reference 1). An outboard profile of the launch vehicle configuration for the AAP-1A mission is presented in Figure 1. The following sections present the required trajectory data associated with the standard and in-plane dispersed trajectories for the northeast launch azimuths.

### 2.1 Standard Trajectories

The standard trajectories correspond to the nominal trajectories documented in Volume 1 of this Technical Note (Reference 2). Shown in Figure 2 are the IIP traces for each launch azimuth. The range safety required data for these trajectories are contained on the cape magnetic tape (CCSD Reel No. 4194) in Record 12, Files 2, 5, 8, and 11. A nominal sequence of events is presented in Table 1.

### 2.2 Dispersed Trajectories

Listed below are the combined off-nominal parameter variations about the respective standard trajectories which define the in-plane dispersed trajectories. Figure 3 presents the annual wind profile envelopes, as documented in Reference 3, which are applicable to the northeast launch azimuths. The range safety data requirements prescribed by the range control office, in connection with the following trajectories, are contained in Record 12, Files 3, 4, 6, 7, 9, 10, 12, and 13 on the cape magnetic tape identified in Section 2.1.

#### 45° Flt. Az. ( $i = 50^\circ$ )

|         |              |                                   |
|---------|--------------|-----------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 45° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 45° TW. |

|         |              |                                   |
|---------|--------------|-----------------------------------|
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 45° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 45° HW. |

#### 51.3° Flt. Az. ( $i = 45^\circ$ )

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 51.3° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 51.3° TW. |

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 51.3° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 51.3° HW. |

#### 57.2° Flt. Az. ( $i = 40^\circ$ )

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 57.2° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 57.2° TW. |

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 57.2° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 57.2° HW. |

66.7° Flt. Az. (i = 35°)

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 66.7° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 66.7° TW. |

|         |              |                                     |
|---------|--------------|-------------------------------------|
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 66.7° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 66.7° HW. |

2.3 Impact of Staging Re-entry Bodies

Impact data for the expended S-IB stage and ullage-rocket cases for both the standard and perturbed trajectories are presented in the following tables and are illustrated in Figure 4. The dotted lines in Figure 4 represent the maximum boundaries of impact points for  $\pm 3\sigma$  performing launch vehicles. These boundaries are symmetrical about the standard and may be applied to any of the trajectories shown. The following data reflect atmospheric re-entry and retro-rocket firing where applicable.

| <u>Trajectory</u> | <u>S-IB Stage</u>          |                             | <u>Time Remaining</u><br>(sec) | <u>Range</u><br>(km) | <u>Range</u><br>(n mi) |
|-------------------|----------------------------|-----------------------------|--------------------------------|----------------------|------------------------|
|                   | <u>Latitude</u><br>(deg N) | <u>Longitude</u><br>(deg W) |                                |                      |                        |

45° Flt. Az. (i = 50°)

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 31.6928 | 76.8514 | 394.8 | 501.3 | 270.7 |
| Maximum  | 31.8322 | 76.6776 | 401.9 | 523.9 | 282.9 |
| Minimum  | 31.5469 | 77.0324 | 382.9 | 477.7 | 257.9 |

51.3° Flt. Az. (i = 45°)

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 31.2979 | 76.4784 | 394.4 | 500.1 | 270.0 |
| Maximum  | 31.4199 | 76.2877 | 401.5 | 522.7 | 282.2 |
| Minimum  | 31.1704 | 76.6775 | 382.5 | 476.4 | 257.2 |

57.2° Flt. Az. (i = 40°)

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 30.8975 | 76.1802 | 394.1 | 499.0 | 269.4 |
| Maximum  | 31.0067 | 75.9660 | 401.1 | 522.8 | 282.3 |
| Minimum  | 30.7890 | 76.3931 | 382.4 | 475.3 | 256.6 |

66.7° Flt. Az. (i = 35°)

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 30.2050 | 75.8030 | 394.1 | 498.2 | 269.0 |
| Maximum  | 30.2816 | 75.5719 | 401.1 | 522.0 | 281.9 |
| Minimum  | 30.1296 | 76.0329 | 382.4 | 474.5 | 256.2 |

Ullage-Rocket Cases

| <u>Trajectory</u>               | <u>Latitude</u><br>(deg N) | <u>Longitude</u><br>(deg W) | <u>Time Remaining</u><br>(sec) | <u>Range</u><br>(km) | <u>Range</u><br>(n mi) |
|---------------------------------|----------------------------|-----------------------------|--------------------------------|----------------------|------------------------|
| <u>45° Flt. Az. (i = 50°)</u>   |                            |                             |                                |                      |                        |
| Standard                        | 31.8492                    | 76.6587                     | 597.2                          | 526.5                | 284.3                  |
| Maximum                         | 32.0401                    | 76.4223                     | 605.6                          | 557.3                | 300.9                  |
| Minimum                         | 31.6622                    | 76.8906                     | 584.3                          | 496.3                | 268.0                  |
| <u>51.3° Flt. Az. (i = 45°)</u> |                            |                             |                                |                      |                        |
| Standard                        | 31.4334                    | 76.2680                     | 596.8                          | 525.1                | 283.5                  |
| Maximum                         | 31.6006                    | 76.0085                     | 605.3                          | 555.9                | 300.2                  |
| Minimum                         | 31.2696                    | 76.5236                     | 583.9                          | 494.7                | 267.1                  |
| <u>57.2° Flt. Az. (i = 40°)</u> |                            |                             |                                |                      |                        |
| Standard                        | 31.0120                    | 75.9561                     | 596.6                          | 523.9                | 282.9                  |
| Maximum                         | 31.1633                    | 75.6626                     | 604.9                          | 556.5                | 300.5                  |
| Minimum                         | 30.8719                    | 76.2307                     | 583.7                          | 493.4                | 266.4                  |
| <u>66.7° Flt. Az. (i = 35°)</u> |                            |                             |                                |                      |                        |
| Standard                        | 30.2842                    | 75.5616                     | 596.6                          | 523.0                | 282.4                  |
| Maximum                         | 30.3908                    | 75.2447                     | 604.9                          | 555.7                | 300.1                  |
| Minimum                         | 30.1865                    | 75.8582                     | 583.8                          | 492.5                | 265.9                  |

#### 2.4 $3\sigma$ Flight Corridor

The pitch plane corridor limits are defined by the respective maximum and minimum flight profiles. S-IVB stage guidance target conditions: inertial velocity ( $V$ ), radius ( $R$ ), flight path angle ( $\gamma$ ), inclination angle ( $i$ ), and argument of descending node ( $\theta_n$ ) for a  $\pm 3\sigma$  vehicle flight profile are virtually unchanged from those of the standard. These conditions along with other pertinent conditions at GCS are presented in Table 2. The  $\pm 3\sigma$  pitch plane flight profile illustrated in Figure 5 is for the  $45^\circ$  flight azimuth ( $i = 50^\circ$ ). These data are deemed typical for the other trajectories as well.

Deviations in pertinent parameters, from the standard, which result from the respective maximum and minimum flight profiles are listed below.

| <u>S-IB/S-IVB Stage Separation</u> | <u>S-IB Stage</u>   |                          |
|------------------------------------|---------------------|--------------------------|
| <u>Inert. Vel. (m/sec)</u>         | <u>Altitude (m)</u> | <u>Impact Range (km)</u> |
|                                    |                     |                          |

#### 45° Flt. Az. (i = 50°)

|         |        |          |      |
|---------|--------|----------|------|
| Maximum | +25.85 | + 842.37 | 22.6 |
|---------|--------|----------|------|

|                                 |        |          |       |
|---------------------------------|--------|----------|-------|
| Minimum                         | -17.80 | -1995.87 | -23.6 |
| <u>51.3° Flt. Az. (i = 45°)</u> |        |          |       |
| Maximum                         | +25.75 | + 845.43 | +22.6 |
| Minimum                         | -17.54 | -1997.43 | -23.7 |
| <u>57.2° Flt. Az. (i = 40°)</u> |        |          |       |
| Maximum                         | +27.96 | + 775.12 | +23.8 |
| Minimum                         | -17.33 | -1986.62 | -23.7 |
| <u>66.7° Flt. Az. (i = 35°)</u> |        |          |       |
| Maximum                         | +27.89 | + 776.56 | +23.8 |
| Minimum                         | -17.09 | -1984.87 | -23.7 |

Trajectory IIP times associated with the overfly of land masses are presented in table 3. Data are shown for the continental land masses of Eurasia, Africa, and South America. All times (seconds) are referenced to lift off.

## 2.5 Downrange Impact and Casualty Probability

Illustrated in Figures 2, 4 and 6 are pertinent range safety data related to the northeast launch azimuths, such as, instantaneous impact point (IIP) traces, S-IB stage and ullage-rocket cases impact, crossrange impact corridors, etc. associated with the various trajectory profiles considered in this study. The lateral impact corridors are approximately  $\pm$  100 km.

The probability of a malfunctioning vehicle impacting on land is calculated as:

### S-IB Stage Flight

$$P_I = P(F)_1 \cdot P(F)_x \cdot P(F)_y$$

### S-IVB Stage Flight

$$P_I = P(S)_1 \cdot P(F)_2 \cdot P(F)_x \cdot P(F)_y$$

where:  $P(S)_1$  = Probability of successful first stage operation.

$P(F)_1$  = Probability of first stage failure.

$P(F)_2$  = Probability of second stage failure.

$P(F)_x$  = Probability of failure in downrange (x) direction.

$P(F)_y$  = Probability of failure in crossrange (y) direction.

The probability of injuring a person downrange is calculated as:

$$P_{IP} = P_I \cdot \frac{N}{A} \cdot L_A$$

where:  $P_I$  = Probability of impact.

$\frac{N}{A}$  = Population Density.

$L_A$  = Lethal area of impacting vehicle:

S-IB Stage powered flight = 37,744 sq. ft.  
S-IVB Stage powered flight = 19,400 sq. ft.

45° Flt. Az. ( $i = 50^\circ$ )

The probability of impact within the range safety lateral corridor for Eurasia is:

$$P_{I_EU} = .957 \cdot .030 \cdot \frac{7.86}{460.20} \cdot 1 = 4.90 \times 10^{-4}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY       | $\Delta t$ | $P_I$                 |
|---------------|------------|-----------------------|
| Great Britain | 0.34       | $2.44 \times 10^{-6}$ |
| France        | 2.40       | $1.50 \times 10^{-4}$ |
| Switzerland   | 0.48       | $2.89 \times 10^{-5}$ |
| Italy         | 0.77       | $4.80 \times 10^{-5}$ |
| Yugoslavia    | 1.04       | $3.24 \times 10^{-5}$ |
| Albania       | 0.22       | $1.37 \times 10^{-5}$ |
| Greece        | 0.27       | $1.68 \times 10^{-5}$ |
| Turkey        | 0.44       | $1.65 \times 10^{-5}$ |
| Cyprus (Is.)  | 0.09       | $6.46 \times 10^{-7}$ |
| Israel        | 0.10       | $6.24 \times 10^{-6}$ |
| Egypt         | 0.04       | $8.95 \times 10^{-8}$ |
| Jordan        | 0.26       | $1.62 \times 10^{-5}$ |
| Saudi Arabia  | 0.97       | $6.05 \times 10^{-5}$ |
| Aden          | 0.08       | $5.00 \times 10^{-6}$ |
| Socotra (Is.) | 0.02       | $9.61 \times 10^{-7}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for Eurasia is:

$$P_{IP_EU} = (4.90 \times 10^{-4}) \cdot 150 \cdot \frac{19,400}{27,878,400} = 5.12 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY       | $\frac{N}{A}$ | $P_{IP}$              |
|---------------|---------------|-----------------------|
| Great Britain | 190           | $3.23 \times 10^{-7}$ |
| France        | 175           | $1.82 \times 10^{-5}$ |

|               |     |                       |
|---------------|-----|-----------------------|
| Switzerland   | 250 | $5.02 \times 10^{-6}$ |
| Italy         | 410 | $1.37 \times 10^{-5}$ |
| Yugoslavia    | 95  | $2.14 \times 10^{-6}$ |
| Albania       | 75  | $7.16 \times 10^{-7}$ |
| Greece        | 95  | $1.11 \times 10^{-6}$ |
| Turkey        | 120 | $1.38 \times 10^{-6}$ |
| Cyprus (Is.)  | 45  | $2.02 \times 10^{-8}$ |
| Israel        | 95  | $4.12 \times 10^{-7}$ |
| Egypt         | 65  | $4.05 \times 10^{-9}$ |
| Jordan        | 25  | $2.82 \times 10^{-7}$ |
| Saudi Arabia  | 2   | $8.42 \times 10^{-8}$ |
| Aden          | 2   | $6.95 \times 10^{-9}$ |
| Socotra (Is.) | 4   | $2.68 \times 10^{-9}$ |

51.3° Flt. Az. ( $i = 45^\circ$ )

The probability of impact within the range safety lateral corridor for Eurasia - Africa is:

$$P_{I_{EU-A}} = .957 \cdot .030 \cdot \frac{6.76}{460.20} \cdot 1 = 4.22 \times 10^{-4}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY        | $\Delta t$ | $P_I$                 |
|----------------|------------|-----------------------|
| Spain          | 3.05       | $1.90 \times 10^{-4}$ |
| France         | 0.44       | $7.03 \times 10^{-7}$ |
| Minorca (Is.)  | 0.14       | $1.07 \times 10^{-7}$ |
| Sardinia (Is.) | 0.34       | $1.06 \times 10^{-5}$ |
| Sicily (Is.)   | 0.52       | $8.90 \times 10^{-6}$ |
| Libya          | 0.35       | $2.18 \times 10^{-5}$ |
| Egypt          | 1.04       | $6.49 \times 10^{-5}$ |
| Sudan          | 0.16       | $9.62 \times 10^{-6}$ |
| Saudi Arabia   | 0.14       | $3.34 \times 10^{-6}$ |
| Yemen          | 0.13       | $8.11 \times 10^{-6}$ |
| Aden           | 0.05       | $3.12 \times 10^{-6}$ |
| Somalia        | 0.14       | $8.73 \times 10^{-6}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for Eurasia-Africa is:

$$P_{IP_{EU-A}} = (4.22 \times 10^{-4}) \cdot 150 \cdot \frac{19,400}{27,878,400} = 4.40 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY | $\frac{N}{A}$ | $P_{IP}$              |
|---------|---------------|-----------------------|
| Spain   | 200           | $2.65 \times 10^{-5}$ |
| France  | 200           | $9.78 \times 10^{-8}$ |

|                |     |                       |
|----------------|-----|-----------------------|
| Minorca (Is.)  | 175 | $1.30 \times 10^{-8}$ |
| Sardinia (Is.) | 45  | $3.32 \times 10^{-7}$ |
| Sicily (Is.)   | 300 | $1.86 \times 10^{-6}$ |
| Libya          | 15  | $2.28 \times 10^{-7}$ |
| Egypt          | 75  | $3.39 \times 10^{-6}$ |
| Sudan          | 10  | $6.70 \times 10^{-8}$ |
| Saudi Arabia   | 10  | $2.32 \times 10^{-8}$ |
| Yemen          | 35  | $1.98 \times 10^{-7}$ |
| Aden           | 35  | $7.60 \times 10^{-8}$ |
| Somalia        | 10  | $6.08 \times 10^{-8}$ |

57.2° Flt. Az. (i = 40°)

The probability of impact within the range safety lateral corridor for Europe - Africa is:

$$P_{I_{E-A}} = .957 \cdot .030 \cdot \frac{8.68}{460.20} \cdot 1 = 5.42 \times 10^{-4}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY  | $\Delta t$ | $P_I$                 |
|----------|------------|-----------------------|
| Portugal | 0.70       | $4.15 \times 10^{-5}$ |
| Spain    | 1.28       | $7.59 \times 10^{-5}$ |
| Morocco  | 1.05       | $1.80 \times 10^{-5}$ |
| Algeria  | 2.60       | $1.62 \times 10^{-4}$ |
| Tunisia  | 0.19       | $9.17 \times 10^{-6}$ |
| Libya    | 2.14       | $1.34 \times 10^{-4}$ |
| Egypt    | 0.14       | $4.37 \times 10^{-6}$ |
| Sudan    | 0.95       | $5.93 \times 10^{-5}$ |
| Ethiopia | 0.52       | $3.24 \times 10^{-5}$ |
| Somalia  | 0.11       | $6.86 \times 10^{-6}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for Europe - Africa is:

$$P_{IP_{E-A}} = (5.42 \times 10^{-4}) \cdot 30 \cdot \frac{19,400}{27,878,400} = 1.13 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY  | $\frac{N}{A}$ | $P_{IP}$              |
|----------|---------------|-----------------------|
| Portugal | 90            | $2.60 \times 10^{-6}$ |
| Spain    | 90            | $4.75 \times 10^{-6}$ |
| Morocco  | 50            | $6.25 \times 10^{-7}$ |

|          |    |                       |
|----------|----|-----------------------|
| Algeria  | 20 | $2.26 \times 10^{-6}$ |
| Tunisia  | 2  | $1.28 \times 10^{-8}$ |
| Libya    | 1  | $9.29 \times 10^{-8}$ |
| Egypt    | .5 | $1.52 \times 10^{-9}$ |
| Sudan    | 10 | $4.12 \times 10^{-7}$ |
| Ethiopia | 20 | $4.51 \times 10^{-7}$ |
| Somalia  | 15 | $7.16 \times 10^{-8}$ |

66.7° Flt. Az. (i = 35°)

The probability of impact within the range safety lateral corridor for Africa is:

$$P_{IA} = .957 \cdot .030 \cdot \frac{8.00}{460.20} \cdot 1 = 5.00 \times 10^{-4}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY   | $\Delta t$ | $P_I$                 |
|-----------|------------|-----------------------|
| Sidi Ifni | 0.15       | $1.67 \times 10^{-6}$ |
| Morocco   | 0.85       | $5.30 \times 10^{-5}$ |
| Algeria   | 3.98       | $2.48 \times 10^{-4}$ |
| Niger     | 1.02       | $6.36 \times 10^{-5}$ |
| Chad      | 0.75       | $4.68 \times 10^{-5}$ |
| Sudan     | 1.05       | $6.55 \times 10^{-5}$ |
| Ethiopia  | 0.05       | $1.12 \times 10^{-7}$ |
| Uganda    | 0.04       | $2.04 \times 10^{-8}$ |
| Kenya     | 0.38       | $2.37 \times 10^{-5}$ |
| Somalia   | 0.07       | $3.86 \times 10^{-6}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for Africa is:

$$P_{IP_A} = (5.00 \times 10^{-4}) \cdot 10 \cdot \frac{19,400}{27,875,400} = 3.47 \times 10^{-6}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY   | $\frac{N}{A}$ | $P_{IP}$               |
|-----------|---------------|------------------------|
| Sidi Ifni | 15            | $1.75 \times 10^{-8}$  |
| Morocco   | 10            | $3.69 \times 10^{-7}$  |
| Algeria   | 2             | $3.46 \times 10^{-7}$  |
| Niger     | 2             | $8.86 \times 10^{-8}$  |
| Chad      | 4             | $1.30 \times 10^{-7}$  |
| Sudan     | 15            | $6.84 \times 10^{-7}$  |
| Ethiopia  | 2             | $1.56 \times 10^{-10}$ |
| Uganda    | 15            | $2.13 \times 10^{-10}$ |
| Kenya     | 10            | $1.65 \times 10^{-7}$  |
| Somalia   | 15            | $4.03 \times 10^{-8}$  |

## Section 3.0 - SOUTHEAST LAUNCH AZIMUTHS

The following sections present the required trajectory data associated with the standard and in-plane dispersed trajectories for the southeast launch azimuths.

### 3.1 Standard Trajectories

General information pertaining to this section was presented previously in Section 2.1. The range safety required data for these trajectories are contained on the cape magnetic tape (CCSD Reel No. 0895 ) in Record 12, Files 2, 5, 8, and 11.

### 3.2 Dispersed Trajectories

Listed below are the combined off-nominal parameter variations about the respective standard trajectories which define the in-plane dispersed trajectories. Figure 7 presents the annual wind profile envelopes, as documented in Reference 3, which are applicable to the southeast launch azimuths. The range safety data requirements prescribed by the range control office, in connection with the following trajectories, are contained in Record 12, Files 3, 4, 6, 7, 9, 10, 12, and 13 on the cape magnetic tape identified in Section 3.1.

#### 131.9° Flt. Az. ( $i = 50^\circ$ )

|         |              |                                      |
|---------|--------------|--------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 131.9° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 131.9° TW. |
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 131.9° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 131.9° HW. |

#### 125.3° Flt. Az. ( $i = 45^\circ$ )

|         |              |                                      |
|---------|--------------|--------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 125.3° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 125.3° TW. |
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 125.3° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 125.3° HW. |

#### 118.25° Flt. Az. ( $i = 40^\circ$ )

|         |              |                                       |
|---------|--------------|---------------------------------------|
| Maximum | S-IB Stage:  | +1.7% Thrust & Flow Rate, 118.25° TW. |
|         | S-IVB Stage: | +3.0% Thrust & Flow Rate, 118.25° TW. |
| Minimum | S-IB Stage:  | -2.6% Thrust & Flow Rate, 118.25° HW. |
|         | S-IVB Stage: | -3.0% Thrust & Flow Rate, 118.25° HW. |

110.1° Flt. Az. ( $i = 35^\circ$ )

|         |              |       |                                |
|---------|--------------|-------|--------------------------------|
| Maximum | S-IB Stage:  | +1.7% | Thrust & Flow Rate, 110.1° TW. |
|         | S-IVB Stage: | +3.0% | Thrust & Flow Rate, 110.1° TW. |
| Minimum | S-IB Stage:  | -2.6% | Thrust & Flow Rate, 110.1° HW. |
|         | S-IVB Stage: | -3.0% | Thrust & Flow Rate, 110.1° HW. |

3.3 Impact of Staging Re-entry Bodies

General information pertaining to this section was presented previously in Section 2.3.

| Trajectory | <u>S-IB Stage</u>   |                      | Time<br>Remaining<br>(sec) | Range |        |
|------------|---------------------|----------------------|----------------------------|-------|--------|
|            | Latitude<br>(deg N) | Longitude<br>(deg W) |                            | (km)  | (n mi) |

131.9° Flt. Az. ( $i = 50^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 25.3411 | 76.9954 | 393.3 | 499.6 | 269.8 |
| Maximum  | 25.2053 | 76.8449 | 400.4 | 520.9 | 281.3 |
| Minimum  | 25.4895 | 77.1551 | 381.1 | 476.6 | 257.3 |

125.3° Flt. Az. ( $i = 45^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 25.7381 | 76.6064 | 393.4 | 498.8 | 269.3 |
| Maximum  | 25.6107 | 76.4271 | 400.4 | 521.7 | 281.7 |
| Minimum  | 25.8688 | 76.7844 | 381.4 | 475.8 | 256.9 |

118.25° Flt. Az. ( $i = 40^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 26.2046 | 76.2481 | 393.4 | 497.9 | 268.8 |
| Maximum  | 26.0973 | 76.0526 | 400.4 | 520.8 | 281.2 |
| Minimum  | 26.3148 | 76.4435 | 381.4 | 474.9 | 256.4 |

110.1° Flt. Az. ( $i = 35^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 26.7807 | 75.8956 | 394.3 | 499.1 | 269.5 |
| Maximum  | 26.7054 | 75.6961 | 400.0 | 520.7 | 281.2 |
| Minimum  | 26.8738 | 76.1311 | 381.3 | 473.5 | 255.7 |

| Trajectory | <u>Ullage-Rocket Cases</u> |                      | Time<br>Remaining<br>(sec) | Range |        |
|------------|----------------------------|----------------------|----------------------------|-------|--------|
|            | Latitude<br>(deg N)        | Longitude<br>(deg W) |                            | (km)  | (n mi) |

131.9° Flt. Az. ( $i = 50^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 25.1805 | 76.8254 | 595.6 | 524.3 | 283.1 |
| Maximum  | 24.9979 | 76.6213 | 603.7 | 553.1 | 298.7 |
| Minimum  | 25.3693 | 77.0289 | 582.7 | 495.0 | 267.3 |

125.3° Flt. Az. ( $i = 45^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 25.5965 | 76.4167 | 595.7 | 523.5 | 282.7 |
| Maximum  | 25.4239 | 76.1714 | 603.8 | 554.7 | 299.5 |
| Minimum  | 25.7634 | 76.6448 | 582.9 | 494.0 | 266.7 |

118.25° Flt. Az. ( $i = 40^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 26.0856 | 76.0404 | 595.7 | 522.6 | 282.2 |
| Maximum  | 25.9407 | 75.7728 | 603.8 | 553.8 | 299.0 |
| Minimum  | 26.2264 | 76.2909 | 582.8 | 493.0 | 266.2 |

110.1° Flt. Az. ( $i = 35^\circ$ )

|          |         |         |       |       |       |
|----------|---------|---------|-------|-------|-------|
| Standard | 26.6980 | 75.6897 | 595.4 | 521.6 | 281.6 |
| Maximum  | 26.5858 | 75.3899 | 603.5 | 553.9 | 299.1 |
| Minimum  | 26.8077 | 75.9697 | 582.8 | 491.2 | 265.2 |

3.4  $3\sigma$  Flight Corridor

General information pertaining to this section was presented previously in Section 2.4.

Deviations in pertinent parameters, from the standard, which result from the respective maximum and minimum flight profiles are listed below.

|   | S-IB/S-IVB Stage Separation |              | S-IB Stage        |
|---|-----------------------------|--------------|-------------------|
|   | Inert. Vel. (m/sec)         | Altitude (m) | Impact Range (km) |
| <u>131.9° Flt. Az. (<math>i = 50^\circ</math>)</u>  |                             |              |                   |
| Maximum   | +23.22                      | + 918.62     | +21.3             |
| Minimum   | -15.38                      | -2087.62     | -23.0             |
| <u>125.3° Flt. Az. (<math>i = 45^\circ</math>)</u>  |                             |              |                   |
| Maximum   | +26.08                      | + 833.62     | +22.9             |
| Minimum   | -15.45                      | -2054.30     | -23.0             |
| <u>118.25° Flt. Az. (<math>i = 40^\circ</math>)</u> |                             |              |                   |
| Maximum   | +25.99                      | + 833.81     | +22.9             |
| Minimum   | -15.23                      | -2056.05     | -23.0             |
| <u>110.1° Flt. Az. (<math>i = 35^\circ</math>)</u>  |                             |              |                   |
| Maximum   | +27.38                      | + 782.81     | +21.6             |
| Minimum   | -16.16                      | -2013.05     | -25.6             |

### 3.5 Downrange Impact and Casualty Probability

Pertinent range safety data related to the southeast launch azimuths are illustrated in Figures 2, 4, 6, and 8. General information pertaining to this section was previously presented in Section 2.5.

131.9° Flt. Az. (i = 50°)

The probability of impact within the range safety lateral corridor for South America is:

$$P_{ISA} = .957 \cdot .030 \cdot \frac{93.28}{460.20} \cdot 1 = 5.82 \times 10^{-3}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY            | $\Delta t$ | $P_I$                 |
|--------------------|------------|-----------------------|
| Grand Bahama       | 6.00       | $1.54 \times 10^{-3}$ |
| Great Abaco        | 6.00       | $5.00 \times 10^{-4}$ |
| Nassau             | 2.00       | $6.78 \times 10^{-5}$ |
| Mayaguana          | 7.00       | $7.82 \times 10^{-6}$ |
| Great Inagua       | 9.00       | $1.27 \times 10^{-4}$ |
| Haiti              | 15.00      | $2.57 \times 10^{-4}$ |
| Dominican Republic | 42.00      | $2.62 \times 10^{-3}$ |
| Venezuela          | 33.00      | $2.06 \times 10^{-3}$ |
| Guiana             | 30.00      | $1.87 \times 10^{-3}$ |
| Brazil             | 30.28      | $1.89 \times 10^{-3}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for South America is:

$$P_{IPSA} = (5.82 \times 10^{-3}) \cdot 5 \cdot \frac{19,400}{27,878,400} = 2.02 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY            | $\frac{N}{A}$ | $P_{IP}$              |
|--------------------|---------------|-----------------------|
| Grand Bahama       | 45            | $9.38 \times 10^{-5}$ |
| Great Abaco        | 35            | $2.37 \times 10^{-5}$ |
| Nassau             | 50            | $4.59 \times 10^{-6}$ |
| Mayaguana          | 30            | $1.63 \times 10^{-7}$ |
| Great Inagua       | 40            | $3.54 \times 10^{-6}$ |
| Haiti              | 5             | $8.93 \times 10^{-7}$ |
| Dominican Republic | 45            | $8.21 \times 10^{-5}$ |
| Venezuela          | 2             | $2.87 \times 10^{-6}$ |
| Guiana             | 2             | $2.60 \times 10^{-6}$ |
| Brazil             | 10            | $1.31 \times 10^{-7}$ |

125.3° Flt. Az. ( i = 45° )

The probability of impact within the range safety lateral corridor for South America is:

$$P_{ISA} = .957 \cdot .030 \cdot \frac{35.54}{460.20} \cdot 1 = 2.22 \times 10^{-3}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY            | $\Delta t$ | $P_I$                 |
|--------------------|------------|-----------------------|
| Grand Bahama       | 4.00       | $3.96 \times 10^{-4}$ |
| Great Abaco        | 9.00       | $2.42 \times 10^{-3}$ |
| Mayaguana          | 8.00       | $2.65 \times 10^{-4}$ |
| Dominican Republic | 28.00      | $8.73 \times 10^{-4}$ |
| Puerto Rico        | 33.00      | $1.03 \times 10^{-3}$ |
| Lesser Antilles    | 14.00      | $4.88 \times 10^{-4}$ |
| Guiana             | 13.00      | $8.11 \times 10^{-4}$ |
| Brazil             | 22.54      | $1.41 \times 10^{-3}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for South America is:

$$P_{IPSA} = (2.22 \times 10^{-3}) \cdot 18 \cdot \frac{19,400}{27,878,400} = 2.78 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY            | $\frac{N}{A}$ | $P_{IP}$              |
|--------------------|---------------|-----------------------|
| Grand Bahama       | 45            | $2.42 \times 10^{-5}$ |
| Great Abaco        | 35            | $1.15 \times 10^{-4}$ |
| Mayaguana          | 30            | $1.08 \times 10^{-5}$ |
| Dominican Republic | 45            | $2.73 \times 10^{-5}$ |
| Puerto Rico        | 250           | $1.79 \times 10^{-4}$ |
| Lesser Antilles    | 250           | $8.49 \times 10^{-5}$ |
| Guiana             | 15            | $8.47 \times 10^{-6}$ |
| Brazil             | 20            | $1.96 \times 10^{-5}$ |

118.25° Flt. Az. ( i = 40° )

The probability of impact within the range safety lateral corridor for South America is:

$$P_{ISA} = .957 \cdot .030 \cdot \frac{3.82}{460.20} \cdot 1 = 2.38 \times 10^{-4}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY         | $\Delta t$ | $P_I$                 |
|-----------------|------------|-----------------------|
| Brand Bahama    | 2.06       | $4.17 \times 10^{-5}$ |
| Great Abaco     | 9.00       | $1.04 \times 10^{-3}$ |
| Virgin Is.      | 18.00      | $2.07 \times 10^{-4}$ |
| Lesser Antilles | 18.00      | $9.98 \times 10^{-4}$ |
| Brazil          | 3.82       | $2.38 \times 10^{-4}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for South America is:

$$P_{IP_{SA}} = (2.38 \times 10^{-4}) \cdot 100 \cdot \frac{19,400}{27,878,400} = 1.66 \times 10^{-5}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY         | $\frac{N}{A}$ | $P_{IP}$              |
|-----------------|---------------|-----------------------|
| Grand Bahama    | 45            | $2.54 \times 10^{-6}$ |
| Great Abaco     | 35            | $4.95 \times 10^{-5}$ |
| Virgin Is.      | 250           | $3.59 \times 10^{-5}$ |
| Lesser Antilles | 250           | $1.74 \times 10^{-4}$ |
| Brazil          | 100           | $1.66 \times 10^{-5}$ |

110.1° Flt. Az. (i = 35°)

The probability of impact within the range safety lateral corridor for Africa is:

$$P_{IA} = .957 \cdot .030 \cdot \frac{0.37}{460.20} \cdot 1 = 2.29 \times 10^{-5}$$

The probability of impact for individual countries within the range safety lateral corridor is:

| COUNTRY               | $\Delta t$ | $P_I$                 |
|-----------------------|------------|-----------------------|
| Great Abaco           | 7.93       | $1.19 \times 10^{-4}$ |
| Union of South Africa | 0.37       | $2.29 \times 10^{-5}$ |

The probability of injuring a person as a result of debris impact within the confines of the range safety lateral corridor for Africa is:

$$P_{IP_A} = (2.29 \times 10^{-5}) \cdot 75 \cdot \frac{19,400}{27,878,400} = 1.19 \times 10^{-6}$$

The probability of injuring a person for individual countries within the range safety lateral corridor is:

| COUNTRY               | $\frac{N}{A}$ | $P_{IP}$              |
|-----------------------|---------------|-----------------------|
| Great Abaco           | 35            | $5.62 \times 10^{-6}$ |
| Union of South Africa | 75            | $1.19 \times 10^{-6}$ |

#### Section 4.0 - REFERENCES

- 1) AFETRM 127-1, Safety Range Safety Manual, dated 1 November 1966.
- 2) CCSD TN-AP-67-279, AAP-1A Launch Vehicle Performance and Preliminary Range Safety Analyses Volume 1- Vehicle Performance, dated November 1967.
- 3) MSFC R-AERO-Y-118-66, Cape Kennedy Wind Component Statistics, 0-60 km Altitude, for All Flight Azimuths for Monthly and Annual Reference Periods, dated October 25, 1966.

## Section 5.0 - GOVERNMENT FURNISHED DOCUMENTATION

The Government Furnished Documentation listed below was used in the preparation of this document.

### GOVERNMENT FURNISHED DOCUMENTATION

#### DELIVERABLE ITEM NO. SSR-107

| GPDA NO.          | DATE MSFC APPROVAL                  | DESCRIPTION OF GFD REQ'D.    | IDENTIFICATION OF GFD  |
|-------------------|-------------------------------------|------------------------------|--|
| 0700001<br>Rev. A | October 2, 1967<br>October 11, 1967 | Mission Profile              | Launch from pad 34 into 87 x 140 n. mi. elliptical orbits, using northerly and southerly azimuths for planar flight to orbital inclinations of 35°, 40°, 45°, and 50°. |
| 0700002           | October 2, 1967                     | Mass Characteristics         | CCSD TN-AP-67-186  |
| 0700003           | October 2, 1967                     | Propulsion Data              | CCSD TN-AP-67-186  |
| 0700004           | October 2, 1967                     | Aerodynamic Coefficient Data | CCSD TN-AP-67-182  |

Section 6.0 - DISTRIBUTION

W. H. Mann, Jr.

I-1/1B-E

(1)

L. M. McNair

R-AERO-P

(56 copies, 1 reproducible and  
2 magnetic tapes)

**TABLE 1**  
**SEQUENCE OF EVENTS**

| Event                                  | Time (Sec) |
|--|------------|
| Lift-off                               | 0.0        |
| Initiate Pitch Maneuver                | 10.0       |
| Tilt Arrest                            | 130.3      |
| Inboard Engine Cutoff (IECO)           | 137.3      |
| Outboard Engine Cutoff (OECO)          | 140.3      |
| Physical Separation                    | 141.6      |
| J-2 Engine Start                       | 146.3      |
| Engine Mixture Ratio Stepup            | 147.6      |
| Jettison Ullage Rocket Cases           | 156.3      |
| Jettison LES, Initiate Active Guidance | 175.9      |
| Engine Mixture Ratio Stepdown          | 426.3      |
| J-2 Engine Cutoff                      | 606.5      |
| Time of Epoch                          | 616.5      |

BOOSTER GUIDANCE CUTOFF SIGNAL (GCS) CONDITIONS

Northwest Flight Azimuth

| Flight Azimuth                    | 45°   | 51.3°        | 57.2°        | 66.7°        |
|-----------------------------------|-------|--------------|--------------|--------------|
| Time                              | sec   | 606.51 ± 24  | 606.51 ± 24  | 606.52 ± 24  |
| Inertial Velocity (V)             | m/sec | 7836.40      | 7836.40      | 7836.40      |
| Altitude                          | km    | 169.77       | 169.16       | 167.62       |
| Radius (R)                        | km    | 6539.28      | 6539.27      | 6539.27      |
| Flight Path Angle ( $\gamma$ )    | deg   | 90.00        | 90.00        | 90.00        |
| Latitude                          | deg   | 39.65 ± 0.35 | 37.96 ± 0.29 | 35.99 ± 0.21 |
| Longitude                         | deg   | 65.20 ± 0.59 | 63.87 ± 0.64 | 62.78 ± 0.66 |
| Range                             | km    | 1875.21 ± 65 | 1870.52 ± 65 | 1865.64 ± 64 |
| Inclination (i)                   | deg   | 50.00        | 45.00        | 40.00        |
| Arg. of Desc. Node ( $\Omega_1$ ) | deg   | 154.20       | 148.40       | 141.00       |

TABLE 2

Southeast Flight Azimuths

| Flight Azimuth                    | 131.9° | 125.3°       | 118.25°      | 110.1°       |
|-----------------------------------|--------|--------------|--------------|--------------|
| Time                              | sec    | 606.52 ± 24  | 606.52 ± 24  | 606.52 ± 24  |
| Inertial Velocity (V)             | m/sec  | 7836.40      | 7836.40      | 7836.40      |
| Altitude                          | km     | 162.70       | 162.99       | 163.36       |
| Radius (R)                        | km     | 6539.27      | 6539.27      | 6539.27      |
| Flight Path Angle ( $\gamma$ )    | deg    | 90.00        | 90.00        | 90.00        |
| Latitude                          | deg    | 15.97 ± 0.48 | 17.31 ± 0.44 | 19.02 ± 0.39 |
| Longitude                         | deg    | 68.25 ± 0.35 | 66.84 ± 0.40 | 65.38 ± 0.46 |
| Range                             | km     | 1879.24 ± 65 | 1873.72 ± 65 | 1868.88 ± 65 |
| Inclination (i)                   | deg    | 50.00        | 45.00        | 40.00        |
| Arg. of Desc. Node ( $\Omega_1$ ) | deg    | 28.65        | 34.30        | 41.80        |

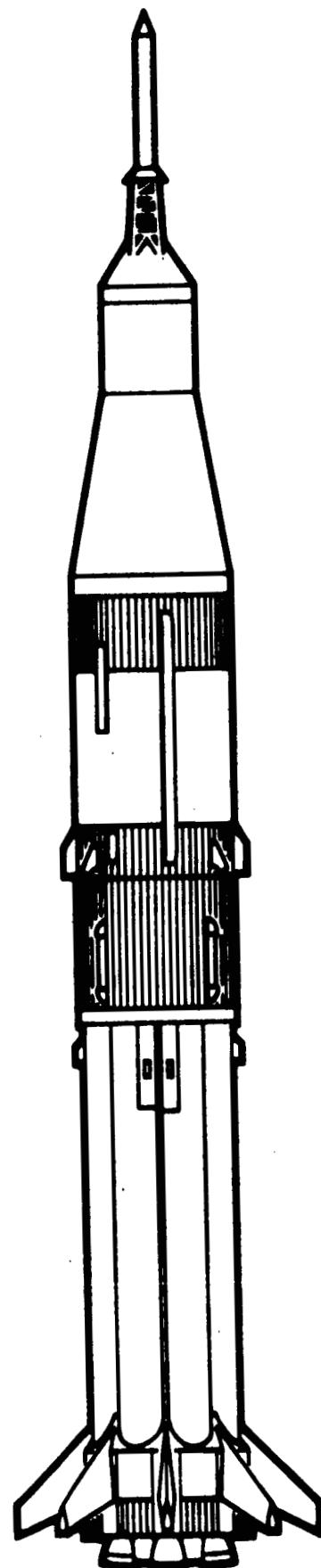
NOTE: V, R,  $\gamma$ , i, and  $\Omega_1$  are S-IVB Stage guidance control cutoff conditions.

TABLE 3

**TRAJECTORY IIP TIMES ASSOCIATED WITH OVERFLY OF LAND MASS  
(Eurasia, Africa, and South America)**

| <u>Trajectory</u>                                   | <u>TB3 (OECO)</u> | <u>Enter<br/>Land Mass</u> | <u>Leave Land Mass</u> |
|---|-------------------|----------------------------|------------------------|
| <u>45° Flt. Az. (<math>i = 50^\circ</math>)</u>     |                   |                            |                        |
| Standard  | 140.32            | 594.21                     | 602.44                 |
| Maximum   | 137.97            | 574.91                     | 582.69                 |
| Minimum   | 144.07            | 616.64                     | 625.56                 |
| <u>51.3° Flt. Az. (<math>i = 45^\circ</math>)</u>   |                   |                            |                        |
| Standard  | 140.32            | 593.51                     | 602.57                 |
| Maximum   | 137.97            | 574.20                     | 582.79                 |
| Minimum   | 144.07            | 616.00                     | 625.73                 |
| <u>57.2° Flt. Az. (<math>i = 40^\circ</math>)</u>   |                   |                            |                        |
| Standard  | 140.32            | 593.91                     | 602.59                 |
| Maximum   | 137.97            | 574.47                     | 582.69                 |
| Minimum   | 144.07            | 616.40                     | 625.73                 |
| <u>66.7° Flt. Az. (<math>i = 35^\circ</math>)</u>   |                   |                            |                        |
| Standard  | 140.32            | 594.55                     | 602.55                 |
| Maximum   | 137.97            | 575.00                     | 582.60                 |
| Minimum   | 144.07            | 617.10                     | 625.69                 |
| <u>131.9° Flt. Az. (<math>i = 50^\circ</math>)</u>  |                   |                            |                        |
| Standard  | 140.32            | 502.00                     | 595.28                 |
| Maximum   | 137.97            | 490.00                     | 576.09                 |
| Minimum   | 144.07            | 520.00                     | 617.78                 |
| <u>125.3° Flt. Az. (<math>i = 45^\circ</math>)</u>  |                   |                            |                        |
| Standard  | 140.32            | 556.00                     | 593.73                 |
| Maximum   | 137.97            | 539.00                     | 574.35                 |
| Minimum   | 144.07            | 575.00                     | 616.00                 |
| <u>118.25° Flt. Az. (<math>i = 40^\circ</math>)</u> |                   |                            |                        |
| Standard  | 140.32            | 589.06                     | 592.88                 |
| Maximum   | 137.97            | 570.00                     | 573.65                 |
| Minimum   | 144.07            | 611.00                     | 615.24                 |
| <u>110.1° Flt. Az. (<math>i = 35^\circ</math>)</u>  |                   |                            |                        |
| Standard  | 140.32            | 602.17                     | 602.54                 |
| Maximum   | 137.97            | 582.26                     | 582.63                 |
| Minimum   | 144.07            | 625.25                     | 625.66                 |

FIGURE 1



CSM CONFIGURATION

SATURN IB-AAP-1A STANDARD TRAJECTORY INSTANTANEOUS IMPACT TRACES

FIGURE 2

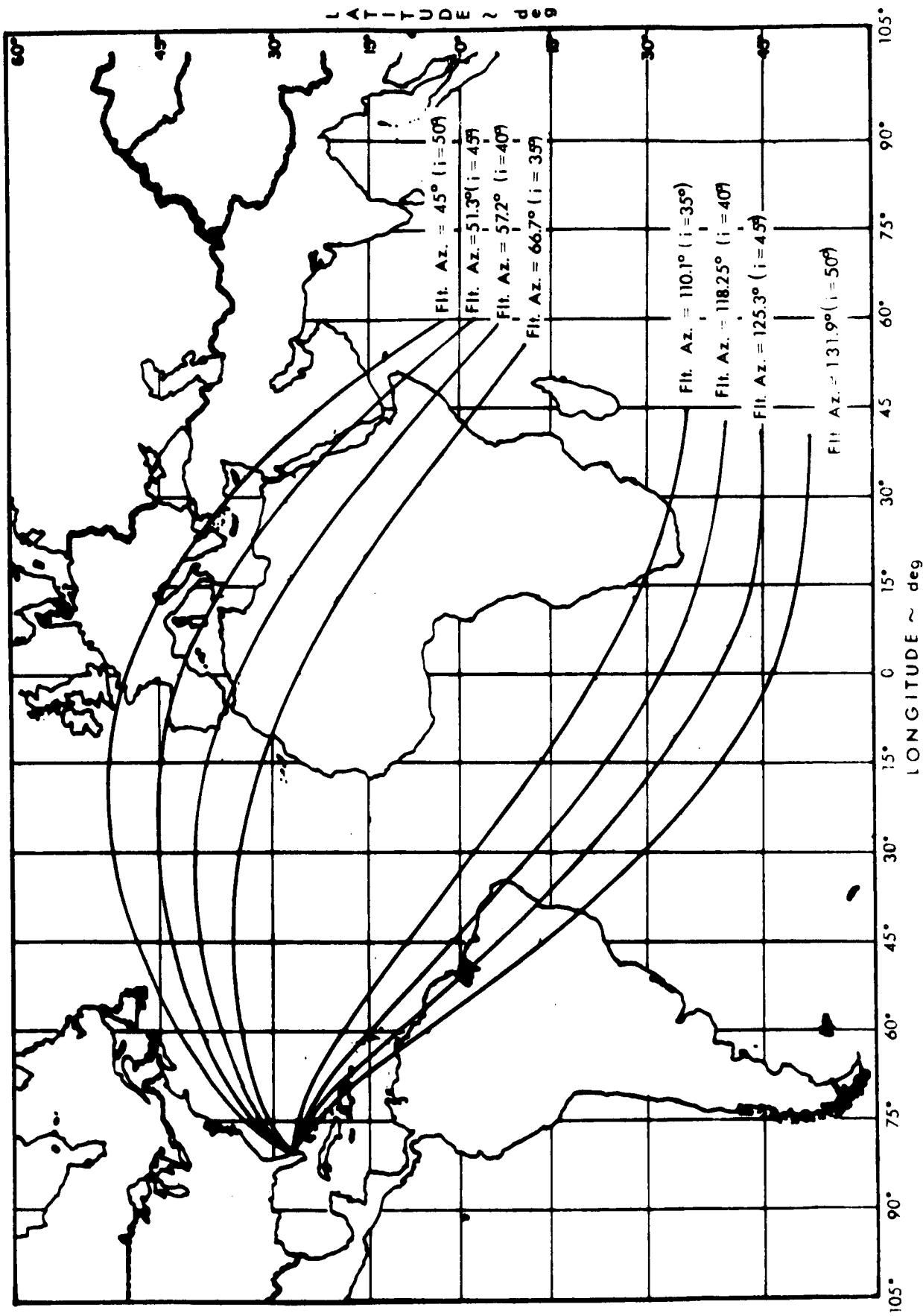


FIGURE 3

ANNUAL WIND PROFILE ENVELOPES  
NORTHEAST FLIGHT AZIMUTHS

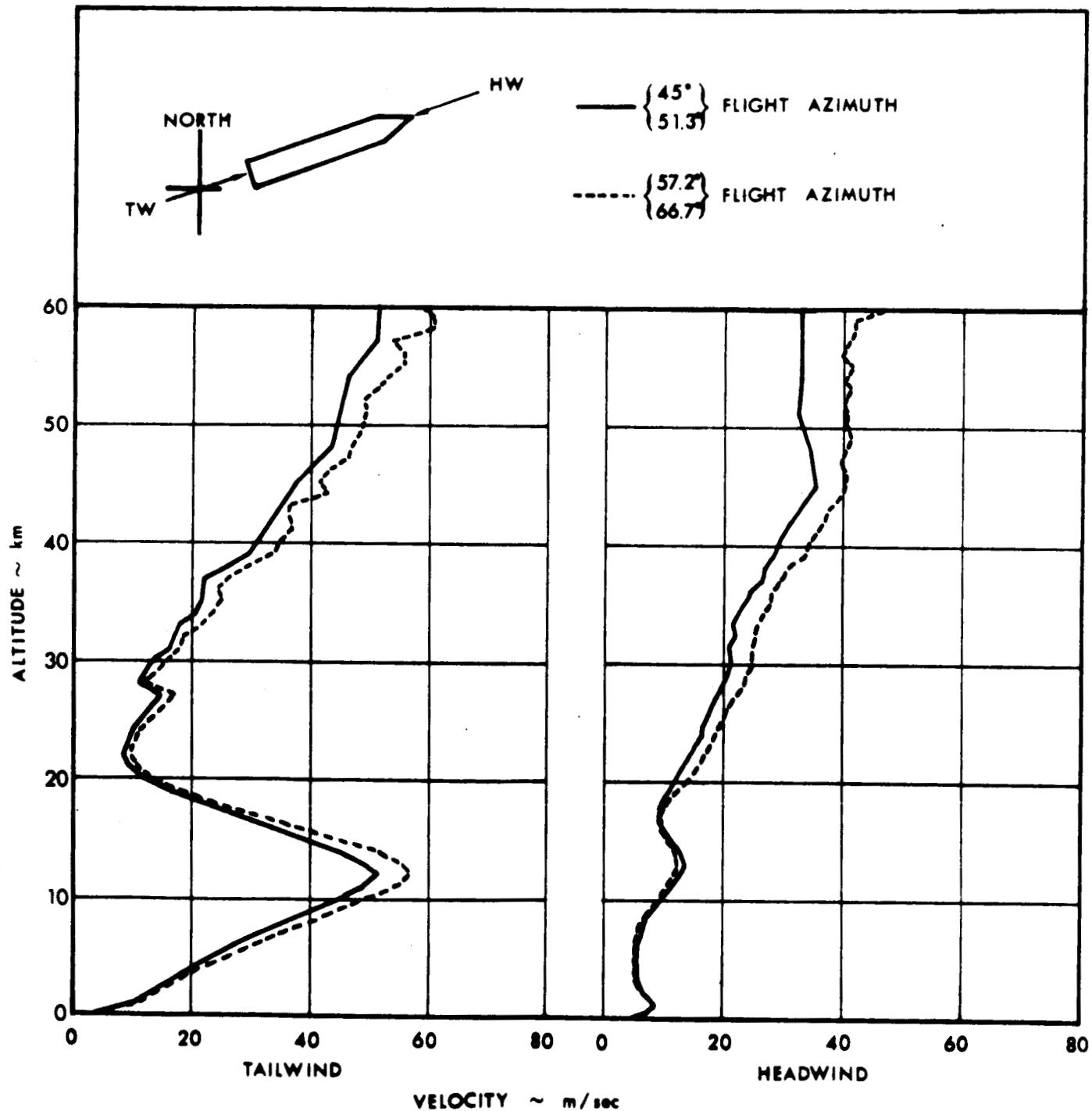


FIGURE 4

## IMPACT DISPERSIONS FOR STAGING RE-ENTRY BODIES

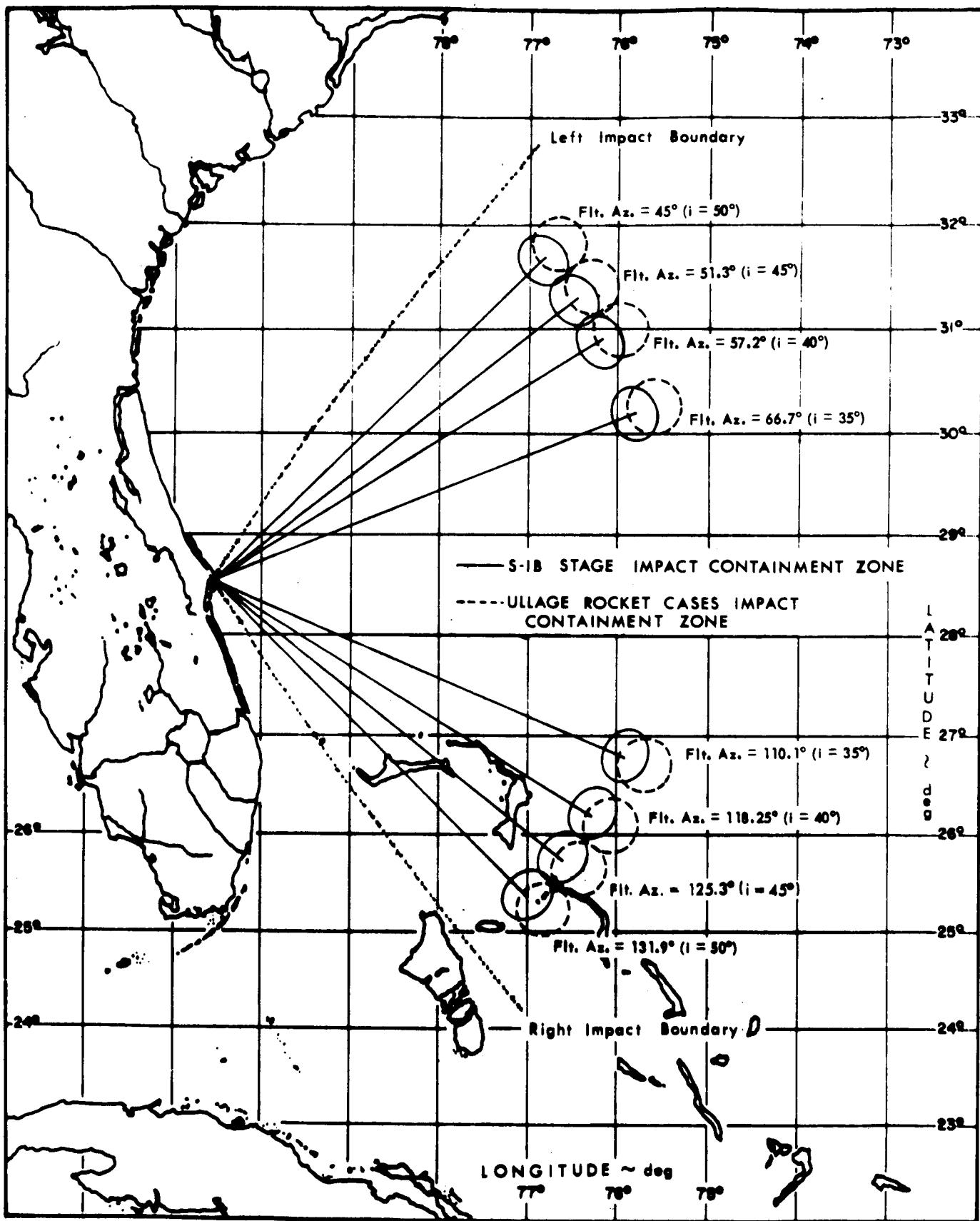


FIGURE 5

## PITCH PLANE FLIGHT PROFILE

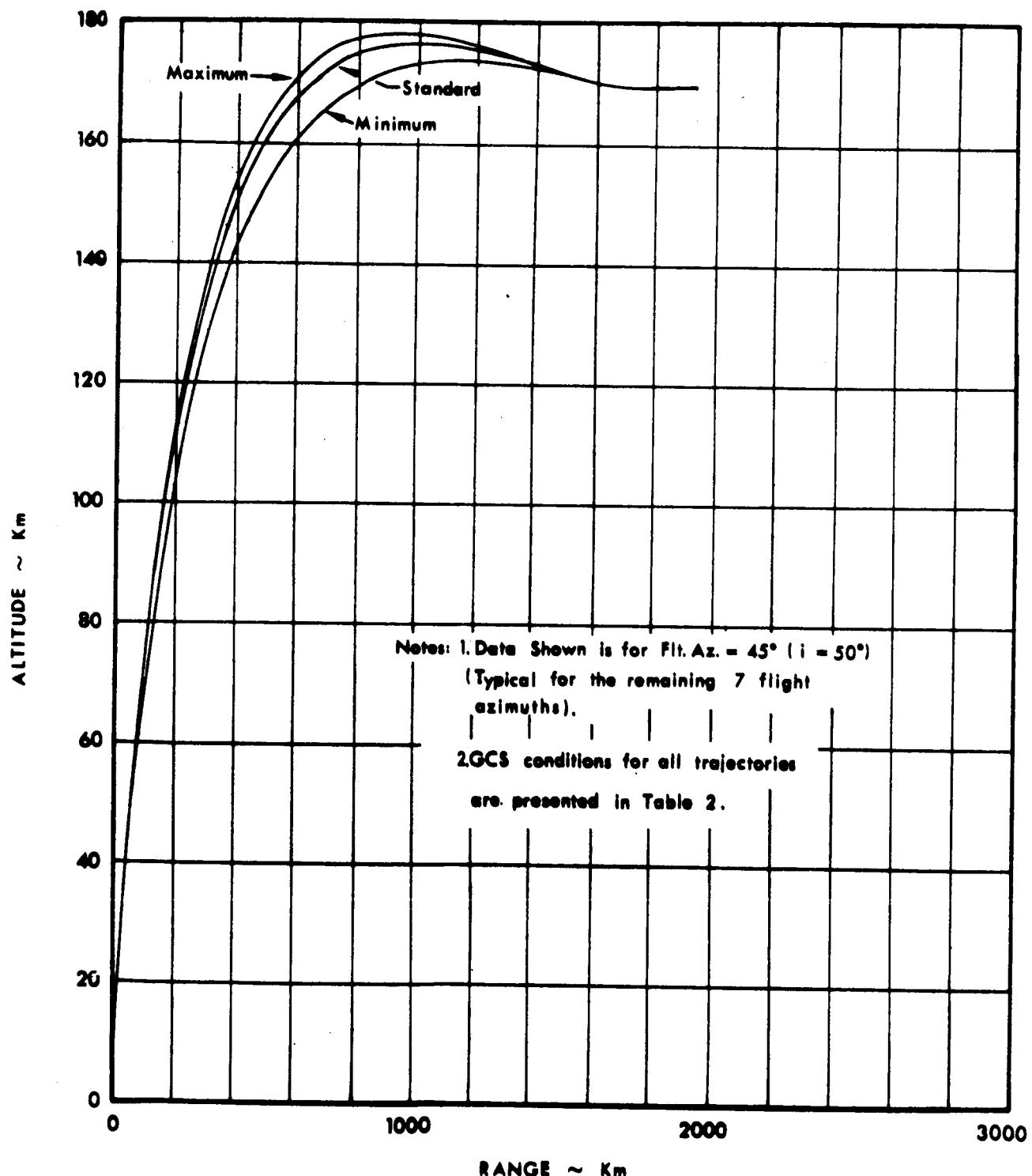


FIGURE 6

**STANDARD TRAJECTORY INSTANTANEOUS IMPACT TRACES AND  
CROSSRANGE CORRIDORS OVER EURASIA AND AFRICA**

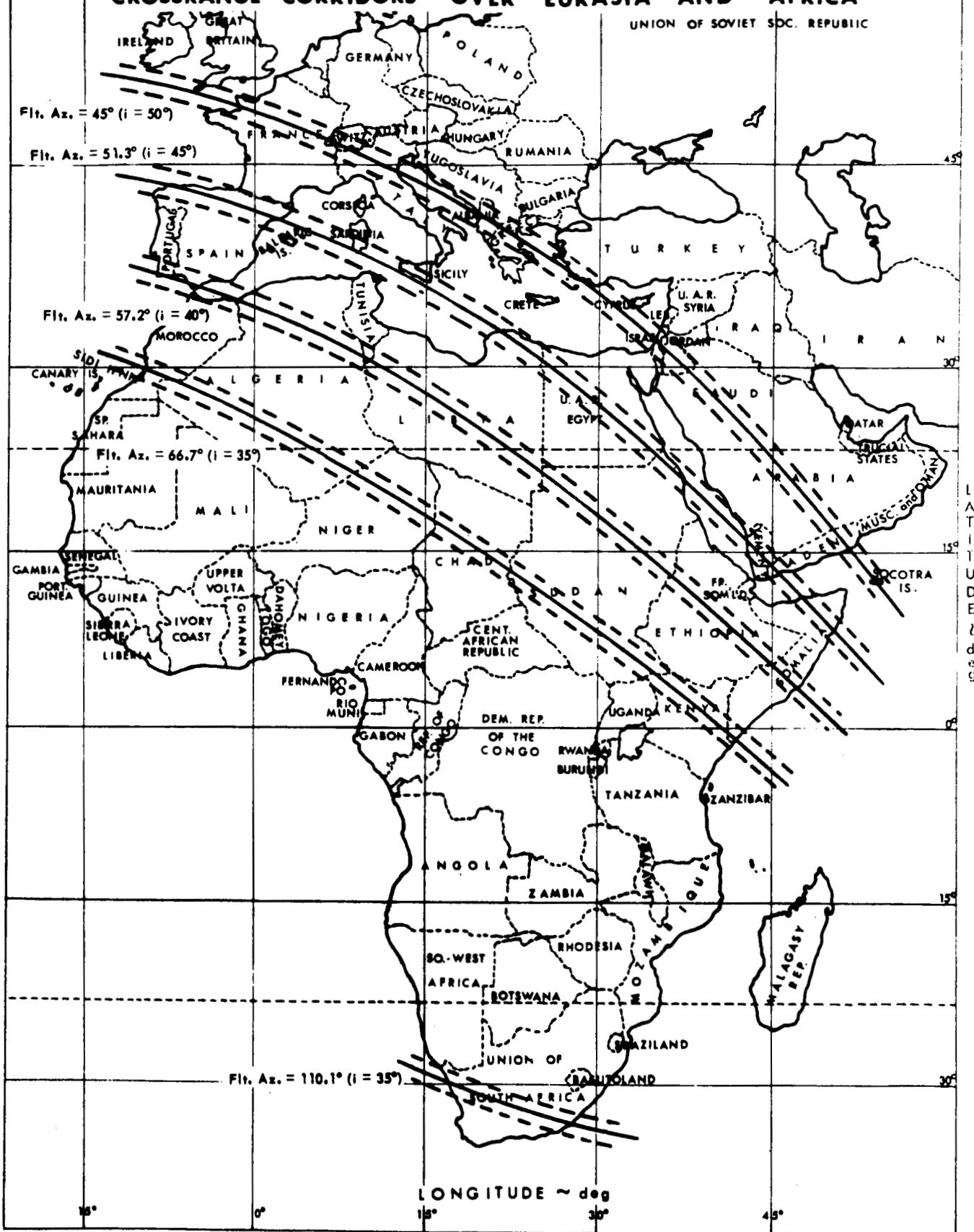


FIGURE 7

ANNUAL WIND PROFILE ENVELOPES  
SOUTHEAST FLIGHT AZIMUTHS

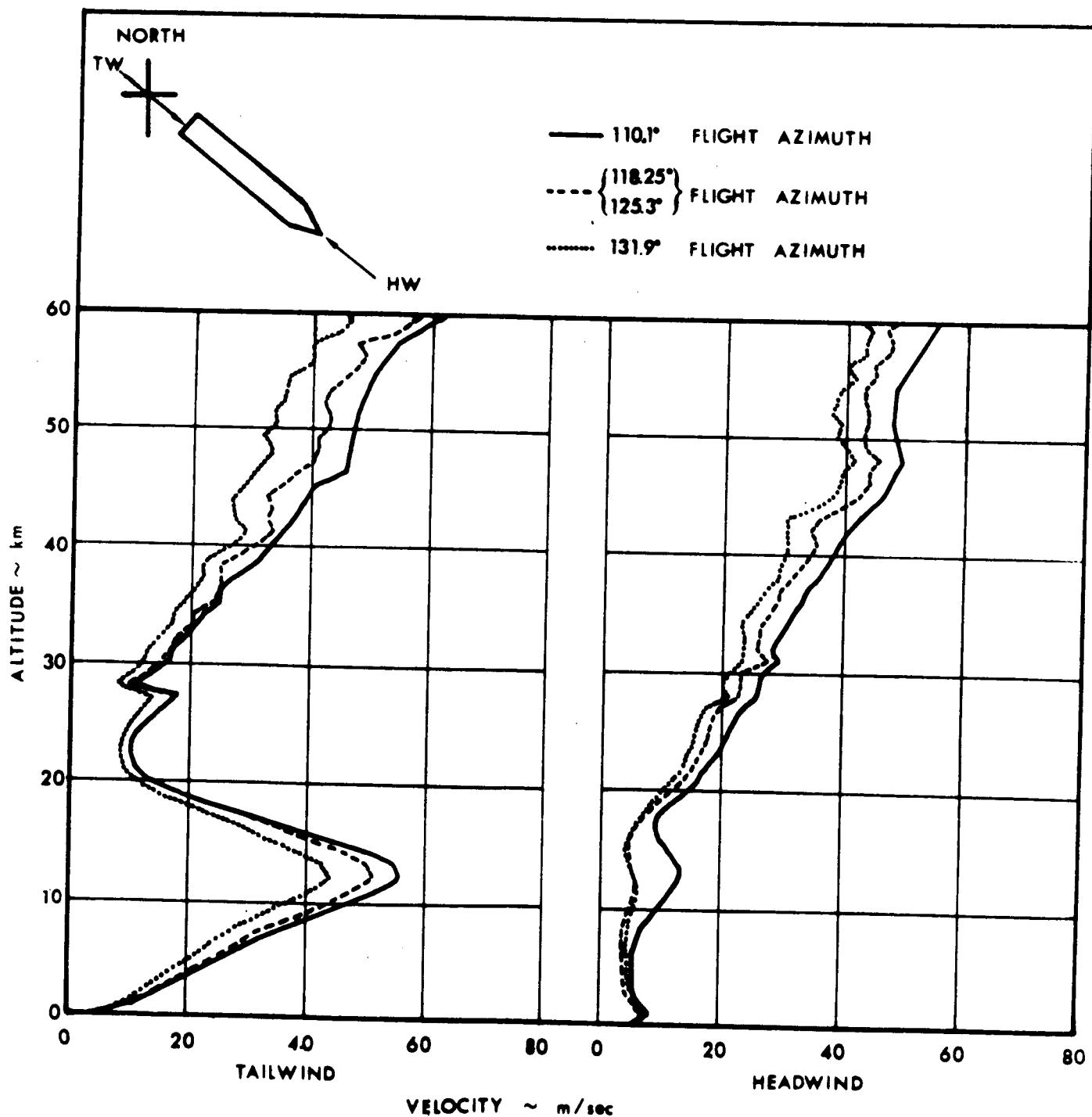


FIGURE - 8

STANDARD TRAJECTORY INSTANTANEOUS IMPACT TRACES  
AND CROSSRANGE CORRIDORS OVER CARIBBEAN ISLANDS  
AND SOUTH AMERICA

